

Generation of Kilowatt/Kilovolt Broadband  
Microwave Bursts with a Single Picosecond  
Photoconductive Switch

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#### ABSTRACT

A single picosecond GaAs photoconductive switch is used to pulse excite a microwave resonant cavity, generating various microwave waveforms. The generation of over 7 kW, with peak to peak voltage over 1.2 kV, of broadband microwave bursts is demonstrated.

#### INTRODUCTION

In the last few years, there has been a great interest in the generation of coherent microwave pulses using ultrashort optical pulses (1-4). These techniques use optical pulses to trigger photoconductive switches, thus allowing picosecond synchronization of the generated microwave pulses. However, drawbacks of the exported methods are i) the low voltage and power outputs (1,2), and ii) the large number of photoconductive switches to be triggered (3,4). Earlier we demonstrated conversion of DC energy to single frequency RF energy, albeit at low voltage and power, using a single switch and a coaxial resonant cavity (5). In this paper we show the versatility of this technique. Among the different waveforms generated, we have produced over 7 kilowatts of broadband, single cycle, microwave pulses of peak to peak voltage of over 1.2 kV with over 50% energy conversion efficiency.

#### EXPERIMENTAL SYSTEM

Schematic of the experimental arrangement is shown in Fig. 1. Coaxial slotted lines were used as quarter wave resonant cavities. Specifically, a 25 cm long HP slotted line cavity, resonating at 300 MHz, and 9 cm long homemade cavity, resonating at 1 GHz, were used. These resonant frequencies are for high Q operation of the cavities. An active-passive mode-locked Nd:YAG laser is used to generate  $\sim 1$  mJ of 1.06  $\mu\text{m}$  radiation, of 100 picosecond pulsewidth, with repetition rate of 1 Hz, to trigger the GaAs switch. The performance of GaAs switches were tested, under DC bias of up to 4 kV, with 1.06  $\mu\text{m}$  pulses for several thousand consecutive shots without any observable degradation in performance.

Activating the GaAs switch by the optical pulse generates a rectangular electric pulse of at most

half the DC charged voltage. The electric pulse excites the resonant cavity through coupling element  $A_1$ . Coupling element  $A_2$  allows the extraction of the generated microwaves from the excited cavity, to be observed by a 1 ns risetime storage scope. Two important and useful parameters that control the waveform, and hence the frequency distribution, of the generated microwaves are i) strength of the coupling provided by  $A_1$  and  $A_2$ , and ii) length of the coaxial line  $C_2$  connecting the GaAs switch to  $A_1$ .

In Fig. 2 we show a typical electric pulse ( $\approx 1.25$  kV in magnitude and 2 ns in duration) used to excite the cavities. The width of the pulse is determined by the length of the charged coaxial line  $C_1$ . The rise time is determined by that of the optical trigger pulse.

#### RESULTS

In Fig. 3 we show the effects of coupling ( $A_1$  and  $A_2$ ) and the length of  $C_2$ . The generated waveform using the 300 MHz cavity, is due to "strong" couplings at  $A_1$  and  $A_2$ . A strong coupling is obtained by directly connecting the center wire of an input/output coaxial line to the center wire of the coaxial resonant cavity. The generated waveform can be explained as follows; some of the incident voltage pulse on  $A_1$  excites the cavity, while some is reflected with a change in sign (since the effective impedance of  $A_1$  is less than the characteristic impedance of  $C_2$ ). The reflected pulse suffers an open circuit reflection at the switch (thus keeping the same sign) and is incident on  $A_1$  repeating the above process. The ratio of the magnitudes of successive pulses is constant, and depends on the coupling strength. The time between successive pulse excitations is given by twice the travel time in the length of  $C_2$  (20 ns round trip time in this case). Note that the first cycle has a peak to peak voltage of  $\approx 1.2$  kV, and that the peak power is over 7 kWatts. The energy conversion efficiency, including all the reflected pulses, is over 50%.

In Fig. 4 we show the effect of changing the couplings and the length of  $C_2$ . Intermediate connection for  $A_2$  is used to excite the 1 GHz cavity, together with a 5 ns (double travel time) long  $C_2$ . Note the relatively larger voltages of the reflected pulses due to the weak coupling at  $A_1$ .

In Fig. 5 we show the waveform generated by the 1 GHz cavity with strong couplings and with a  $\approx 0.5$  ns (double travel time) long  $C_2$ . Note that the width of the generated single cycle pulse is larger than the period of the resonance frequency. There are several reasons for this, the most important of which are; i) the nonzero (0.5 ns) time shift between the (successive) added microwave pulses, ii) the loading of the cavity, and iii) the finite risetime of the scope. The waveform generated by the 300 MHz cavity with strong couplings and with a 0.5 ns long  $C_2$  is shown in Fig. 6.

Finally, a relatively high Q factor is obtained for the cavity when the coupling is weak (loop antennae for  $A_1$  and  $A_2$ ). In this case the triggered electrical pulse excites the cavity at its resonant frequency through  $A_1$ , while  $A_2$  allows the extraction of the generated narrow band microwaves. In Fig. 7 we show the observed waveform for the 1 GHz cavity when  $C_2$  is  $\approx 5$  ns long. Note that over 100 mW of 1 GHz RF is generated, with an estimated bandwidth of less than 10 MHz. The modulated envelope is due to beating between the cavity resonant frequency and the length of  $C_2$ . The nonzero dip of the envelope is caused by the relatively long lifetime of the switch (few ns) when excited by a  $1.06\mu\text{m}$  trigger pulse. This "smears" the effective length of  $C_2$  and hence affects the beating with the cavity resonance frequency. Indeed we have observed a zero dip in the envelope when a short lifetime switch is used (e.g. Cr doped GaAs or  $0.53\mu\text{m}$  trigger pulse.). Unfortunately the use of  $0.53\mu\text{m}$  to trigger high voltage pulses is not practical (6).

The use of spectrum analysers, to examine the frequency distribution of the high voltage high power microwave bursts (Figs. 3-6), is not feasible due to the short duration of the bursts and their low repetition rate. However, more than qualitative information can be obtained by theoretical methods (7). The calculated frequency distribution of the power in single cycle (with positive and negative parts, as in Figs. 5,6) electrical pulses, with a period of  $\tau$ , shows that the main lobe extends up to  $2/\tau$ . The significance of this is evident once one realizes that, similar calculations for one sided electrical pulses (as in Fig. 2) show that the main lobe extends up to  $1/\tau$  only. The frequency distribution for the waveforms in Figs. 3,4 is given by that for a single pulse divided by  $[1+a^2-2a \cos(2\pi ft_g)]$  where  $a$  is negative of the ratio of magnitudes of successive pulses (this depends on the coupling strength) and  $t_g$  is the separation between successive pulses (round trip length of  $C_2$ ).

#### CONCLUSION

We have shown the versatility of microwave generation, through the excitation of a resonant cavity with a single high voltage pulse, triggered by a photoconductive switch. The high power microwave bursts generated may find important applications in high resolution phased array radar operation.

#### ACKNOWLEDGMENTS

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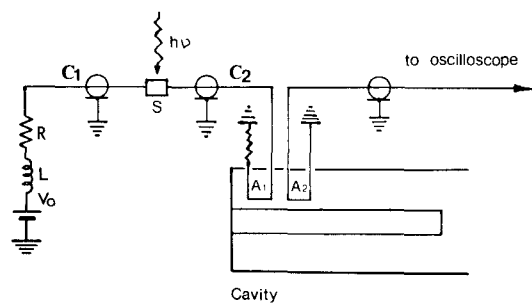


Fig. 1 Schematic of the experimental arrangement. S is GaAs photoconductive switch,  $A_1$  and  $A_2$  are input/output cavity coupling elements.  $C_1$  and  $C_2$  are coaxial cables. The resistance (R) and inductance (L) provide isolation between the DC power supply and the charged line  $C_1$ .

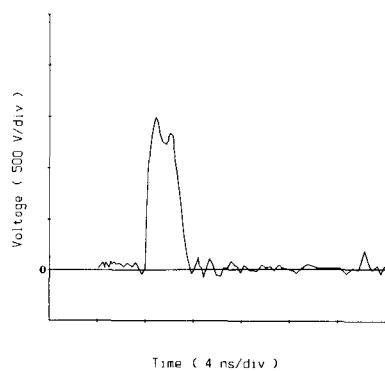


Fig. 2 Typical electric pulse, generated by optically triggering the photoconductive switch, used to excite the cavities.

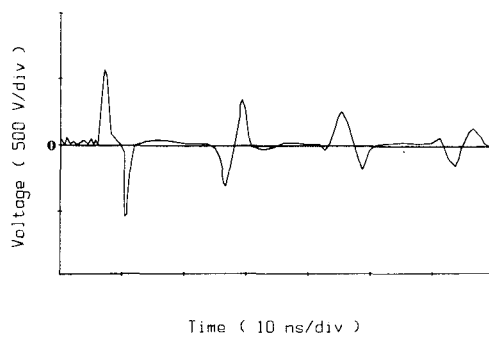


Fig. 3 Microwave pulse generated using the 300 MHz cavity with strongly coupled  $A_1$  and  $A_2$  (see text for definition of coupling strength) and 20 ns (round trip) long  $C_2$ .

Fig. 4 Microwave pulse generated using the 1 GHz cavity with intermediate coupling and 5 ns long  $C_2$ .

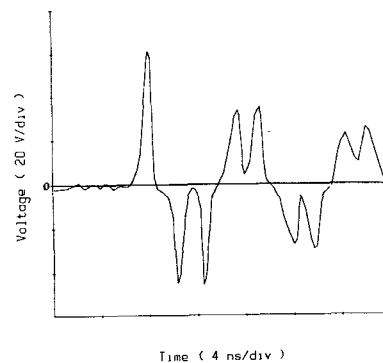


Fig.5 Microwave pulse generated using the 1 GHz cavity with strong coupling and  $\sim 0.5$  ns long  $C_2$ .

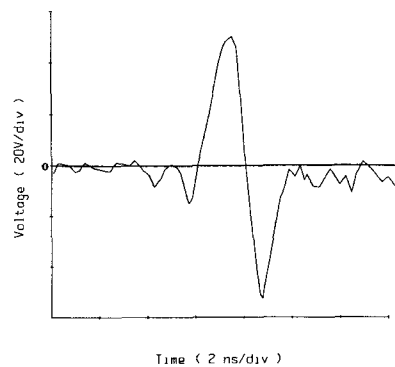


Fig. 6 Microwave pulse generated using the 300 MHz cavity with strong coupling and  $\sim 0.5$  ns long  $C_2$ .

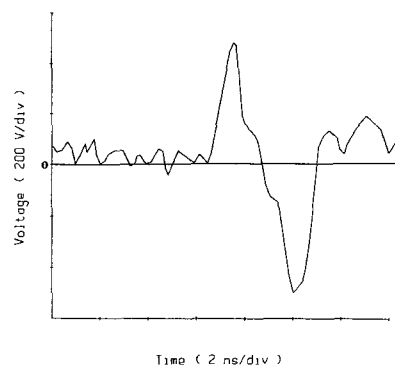


Fig. 7 Microwave generation using the 1 GHz cavity with weak coupling and  $\sim 5$  ns long  $C_2$ . ( 2V / vert. div. , 10 ns / hor. div. )

